

**SFERA-III**

**Solar Facilities for the European Research Area**



IRES 2022 Conference - SFERA III Workshop

*Towards a fair evaluation of Thermal Energy Storage prototypes - Guidelines for CSP applications*

## Case study on latent heat storage

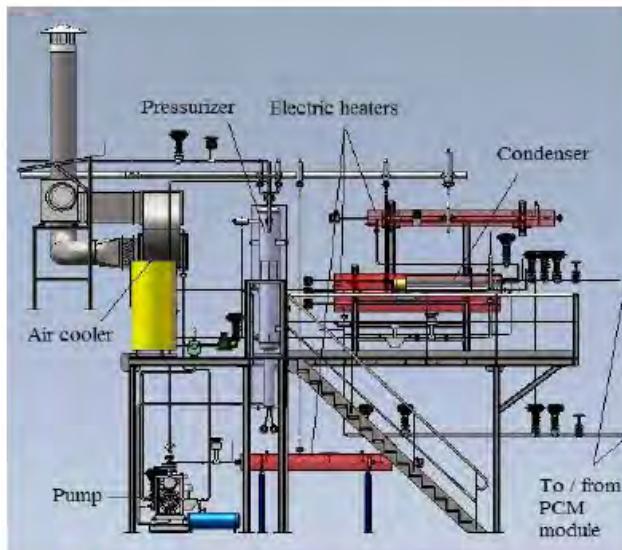
*Pierre Garcia, CEA-LITEN*

JOINT RESEARCH ACTIVITIES



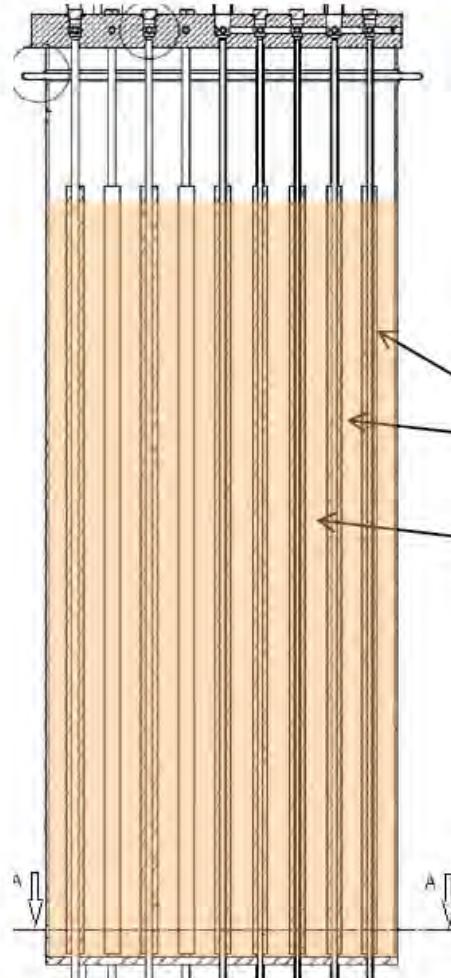
THIS PROJECT HAS RECEIVED FUNDING FROM THE EUROPEAN UNION'S HORIZON 2020 RESEARCH AND INNOVATION PROGRAMME UNDER GRANT AGREEMENT NO 823802

- Thermal Storage is a critical issue for industrial processes using steam as HTF
  - Latent Heat Thermal Energy Storage (**LHTES**) may be required
  - Shell-and-tubes storage with Phase Change Material (**PCM**)
    - Low thermal conductivity → Need of heat transfer enhancement methods on the PCM side
- LHASSA experimental facility at the CEA Grenoble
  - High pressure water-steam closed loop
  - Operating conditions similar to those of CSP DSG plants (145 bar, 350 °C)



*PCM tubes & inserts*

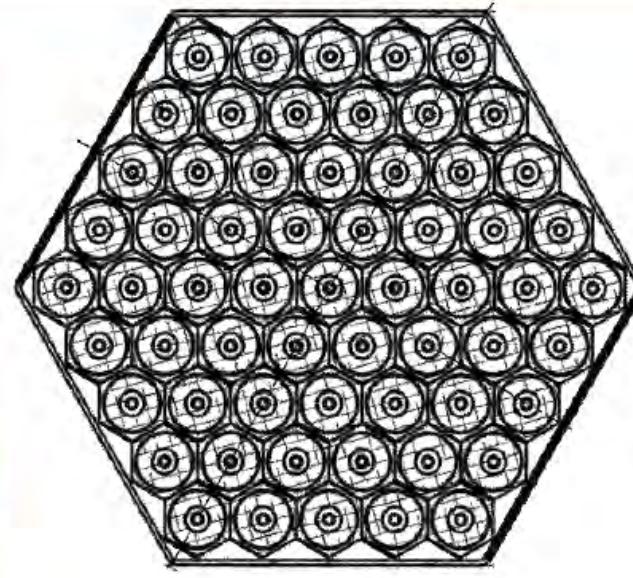
*PCM module  
(6,3 tons of NaNO<sub>3</sub>)*



Vertical bundle of parallel tubes with high pressure steam/water inside and a static PCM volume outside

Finned tubes

PCM volume

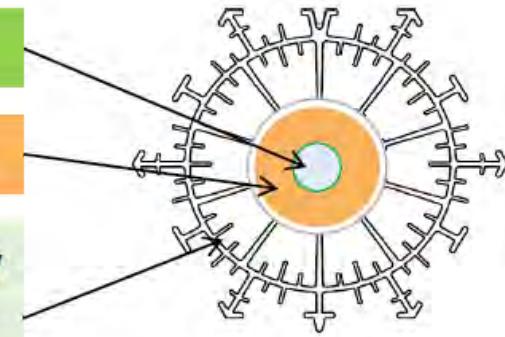


A-A section

Tubes

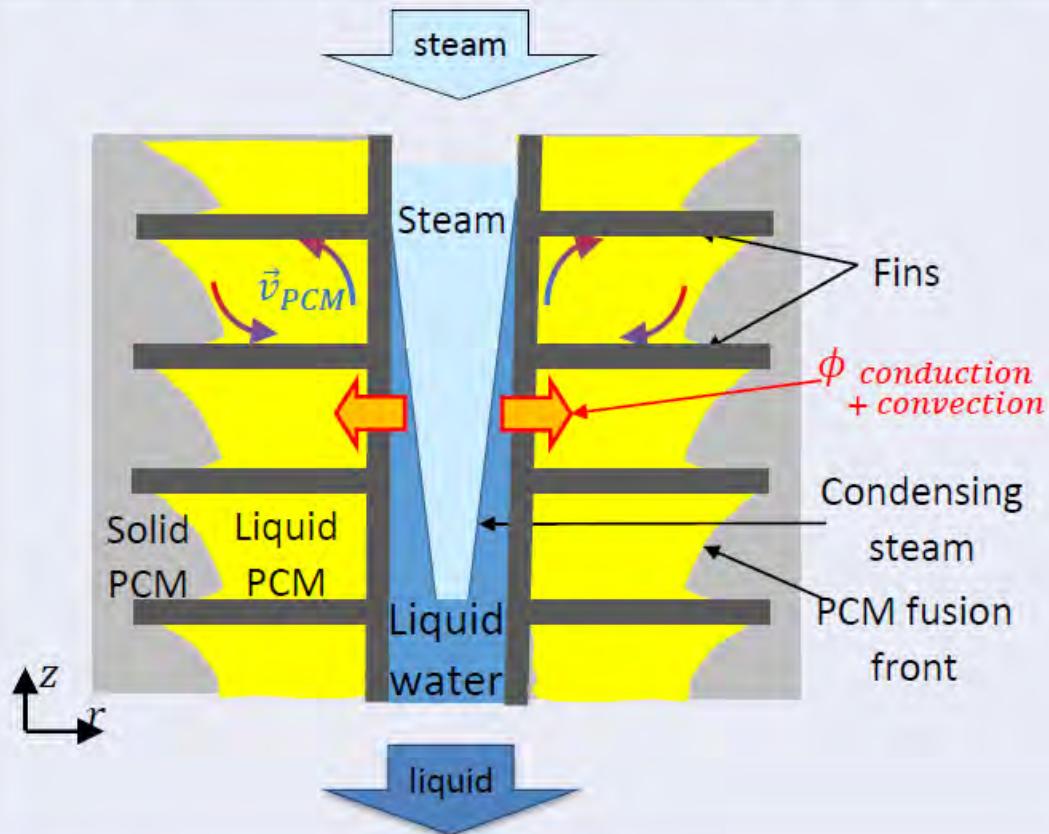
Aluminum fins

Heat transfer enhancement by aluminum inserts around the vertical finned tubes



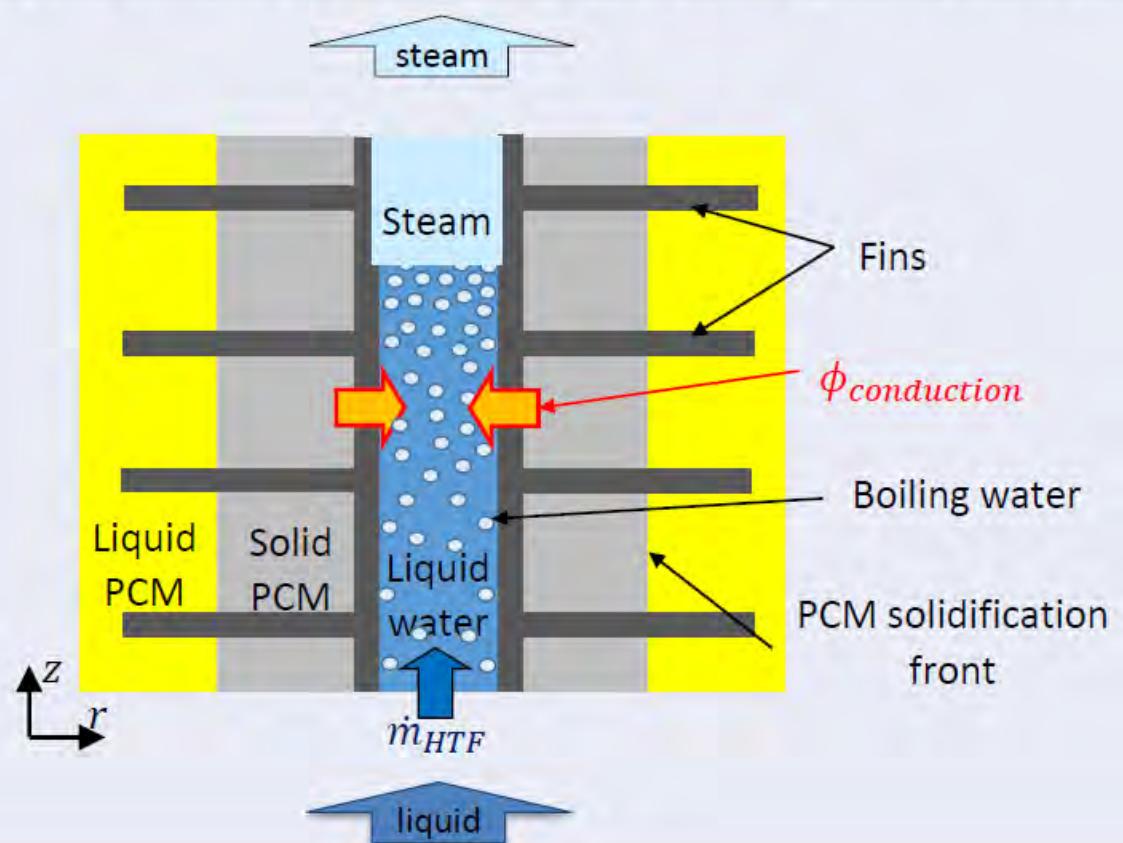
## Charge

Steam condenses causing the melting of the PCM



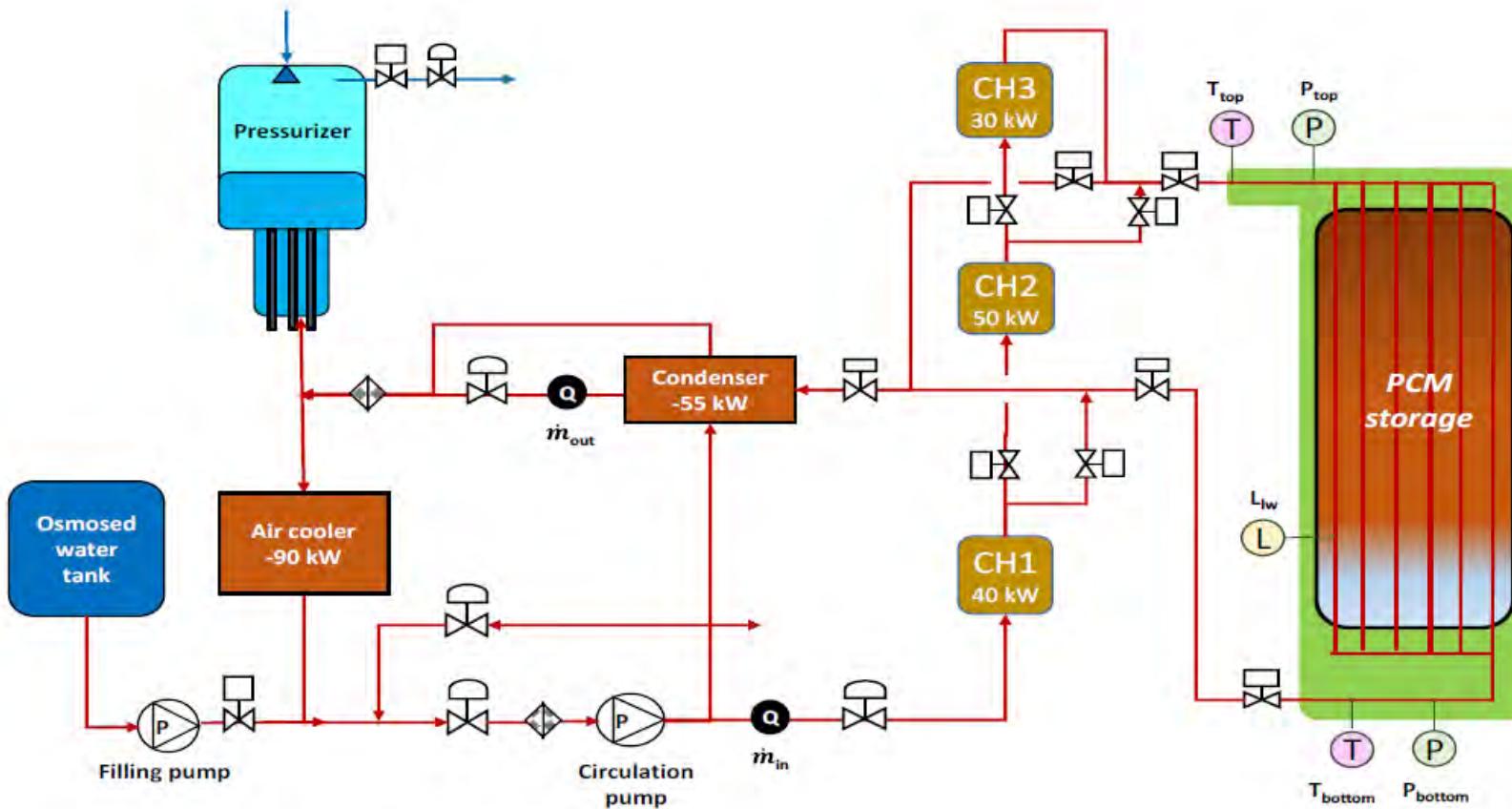
## Discharge

Liquid PCM solidifies causing the evaporation of the liquid water



## Considered system

Tank = storage system, including shell and collectors

**Enthalpy calculations**

- Bottom - liquid water  
 $h_{in} = \text{enthalpy}(T_{in}, P_{in})$
- Top - steam
  - If  $T_{out} > T_{sat} + 2^\circ\text{C}$ ,  $h_{out} = \text{enthalpy}(T_{out}, P_{out})$
  - Else,  $h_{out}$  is calculated from an energy balance at the condenser boundaries
- In charge,  $h_{out} = h_{bottom}$  and  $h_{in} = h_{top}$
- In discharge  $h_{out} = h_{top}$  and  $h_{in} = h_{bottom}$

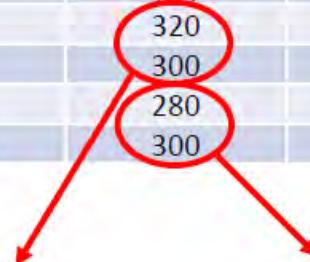
**Theoretical storage capacity ( $SC_{th}$ )**

Includes PCM and metallic parts (tubes, shell, inserts)  
Water volume and thermal insulation are neglected

$$SC_{th} = m_{PCM} H_f + \left( m_{PCM} c_{p_{PCM}} + m_{alu} c_{p_{alu}} + m_{steel} c_{p_{steel}} \right) \cdot (T_{rated,charge} - T_{rated,discharge})$$

Depends on temperature references

| Rated conditions               | Temperature (°C) | Pressure (bara) | Specific enthalpy (kJ/kg) |
|--------------------------------|------------------|-----------------|---------------------------|
| Inlet conditions in charge     | 320              | 100             | 2783                      |
| Outlet conditions in charge    | 300              | 100             | 1343                      |
| Inlet conditions in discharge  | 280              | 80              | 1236                      |
| Outlet conditions in discharge | 300              | 80              | 2786                      |



$$T_{rated,c} = 310^\circ\text{C}$$

$$T_{rated,d} = 290^\circ\text{C}$$

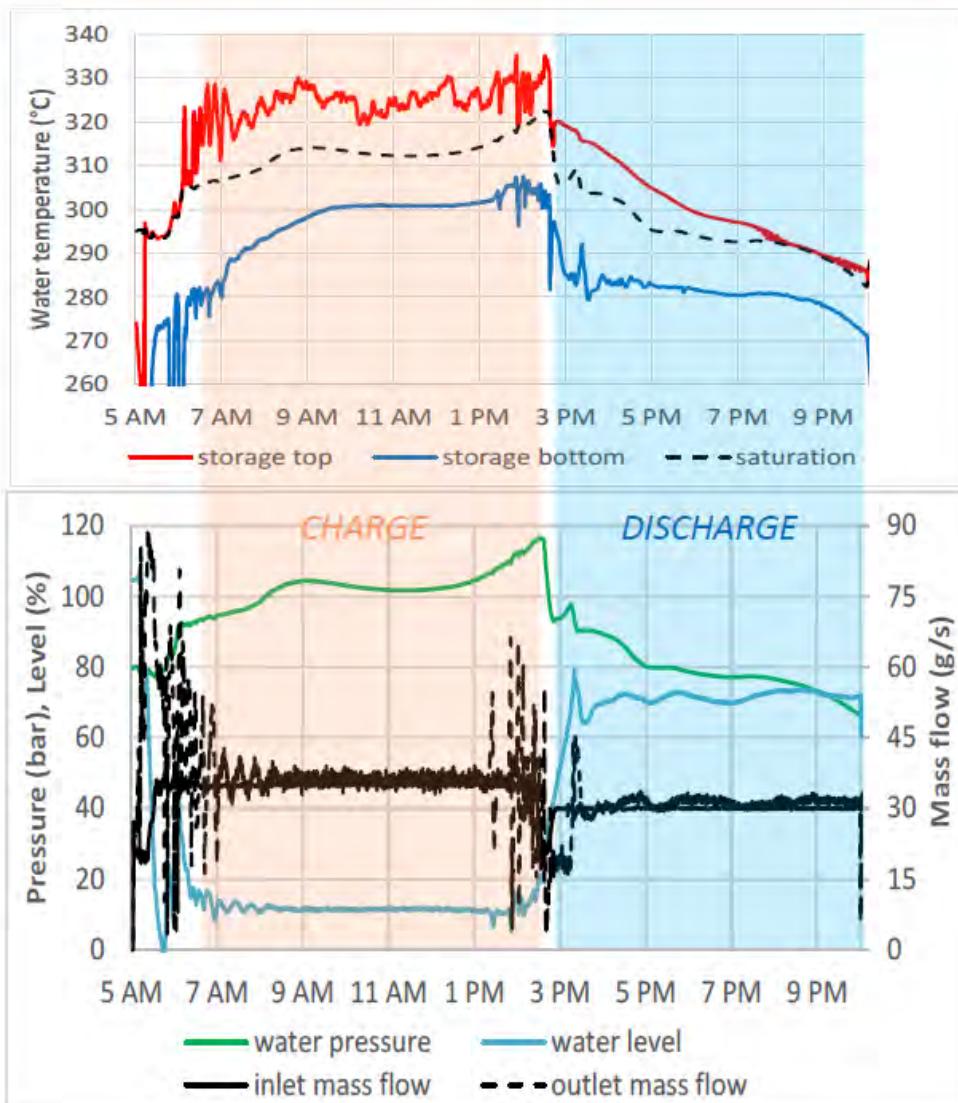
| Metallic parts          | Metal                                 | Steel                  | Aluminum |
|-------------------------|---------------------------------------|------------------------|----------|
|                         | Total mass (kg)                       | 3795 kg                | 1725 kg  |
|                         | Density (kg/m³)                       | 7900                   | 2700     |
|                         | Specific heat (J/kg/K)                | 490                    | 900      |
| PCM<br>(sodium nitrate) | PCM mass (kg)                         | 6330 kg                |          |
|                         | Phase change temperature (°C)         | 306 °C                 |          |
|                         | Heat of fusion (J/kg)                 | 172000 J/kg            |          |
|                         | Mean specific heat (>300 °C) (J/kg/K) | 1655 J/kg/K            |          |
|                         | Density (kg/m³)                       | $\rho(T)$ [Bauer 2012] |          |

|                                     |                            |
|-------------------------------------|----------------------------|
| Total latent heat                   | 302 kWh <sub>t</sub>       |
| Total sensible heat (PCM)           | 58 kWh <sub>t</sub>        |
| Total sensible heat (metal)         | 19 kWh <sub>t</sub>        |
| <b>Theoretical storage capacity</b> | <b>380 kWh<sub>t</sub></b> |
| % sensible heat                     | 20%                        |

- Complete charge and discharge close to rated conditions
    - 17-hour duration
    - Sliding pressure
  - Initial conditions: first cycle
    - HTF flow rate charge
    - HTF flow rate discharge
    - Ambient temperature
  - Operating conditions:

|                           | Criterion               | Threshold value                          | Time    |
|---------------------------|-------------------------|--|---------|
| <b>Start of charge</b>    | Inlet steam temperature | $T_{sat} > T_{pc}$ (306 °C)              | 6:37 AM |
| <b>End of charge</b>      | PCM temperature         | All temperatures in PCM > 306 °C         | 2:37 PM |
| <b>Start of discharge</b> | Inlet water temperature | $T_{sat} < T_{pc}$ (306 °C)              | 2:50 PM |
| <b>End of discharge</b>   | PCM temperature         | $T_{mean} = T_{mean}(t_{start\_charge})$ | 9:26 PM |

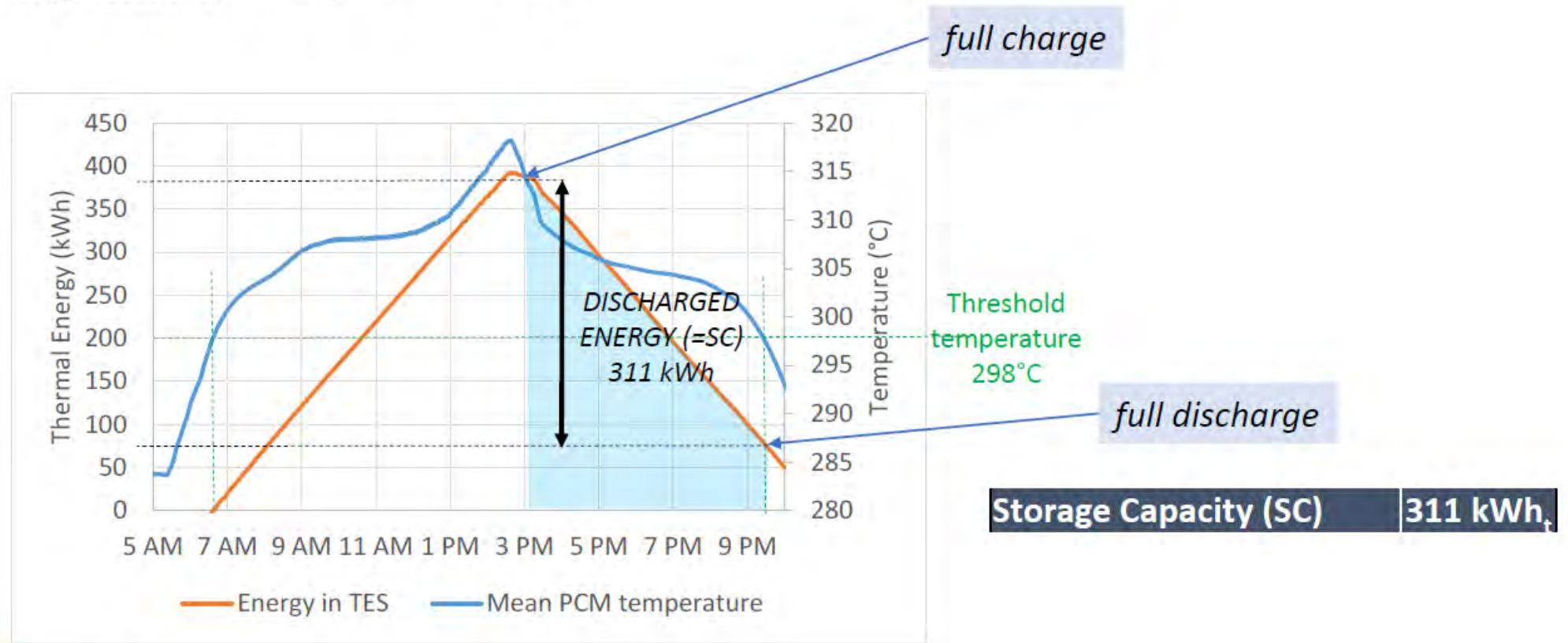
- Start / End criteria: **PCM** mean temperature threshold
    - Temperature on HSM side: inside the tank!
    - To approach cycled conditions



Amount of thermal energy that the TES system can supply by full discharge.

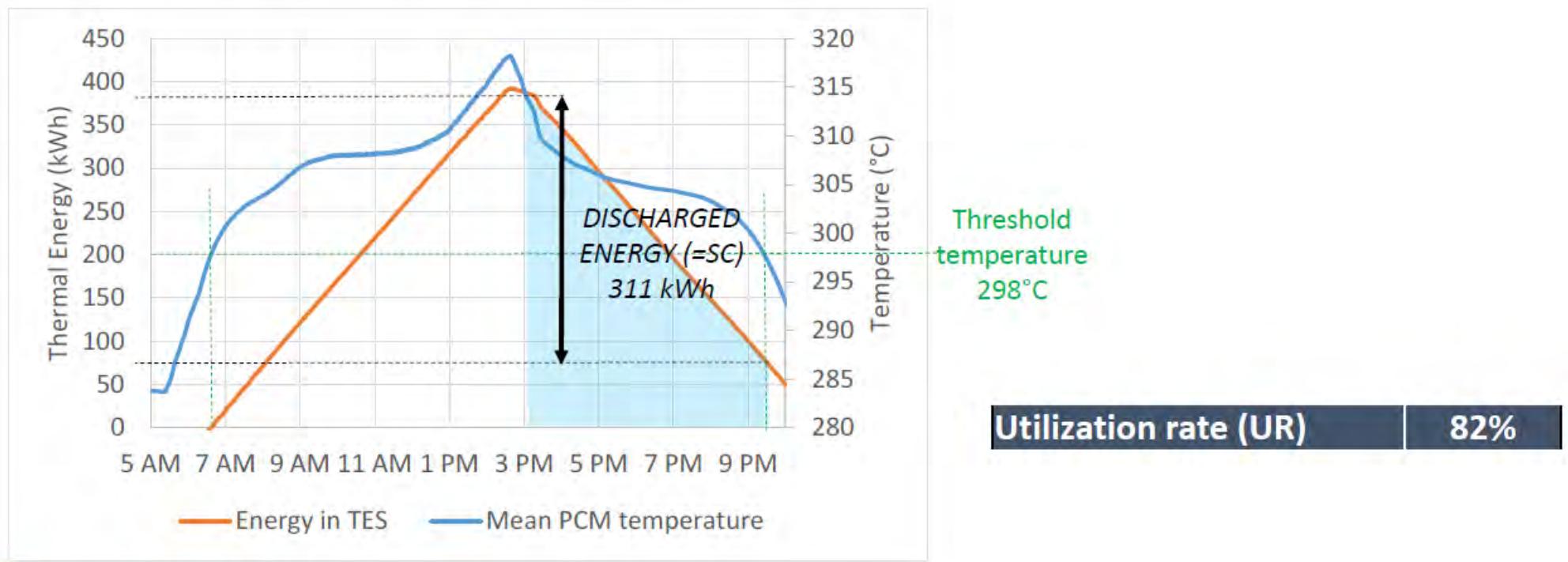
- Calculated on HTF side

$$\bullet \quad SC = \int_{\text{full charge conditions}}^{\text{full discharge conditions}} [\dot{m}_{out} h_{out} - \dot{m}_{in} h_{in}] dt$$



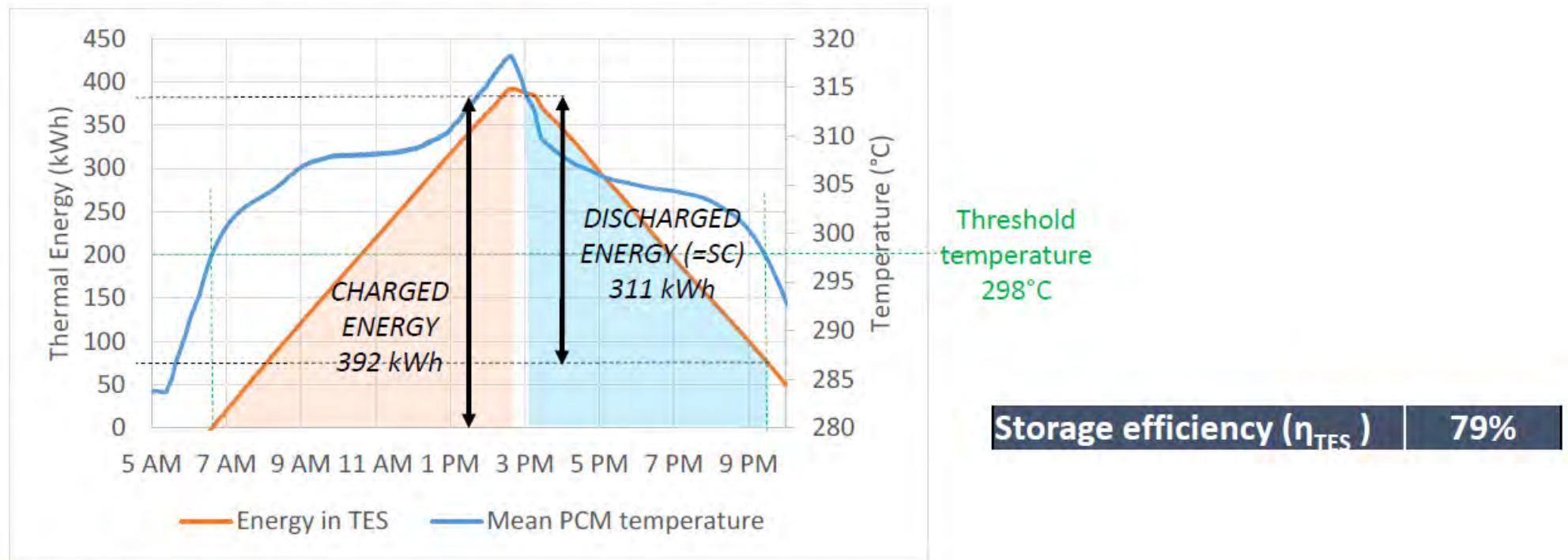
## Ratio of the storage capacity to the theoretical storage capacity of the TES system in rated conditions

- $UR = \frac{SC}{Sc_{th}}$
- With SC calculated on HTF side
- With  $Sc_{th}$  calculated on storage materials side



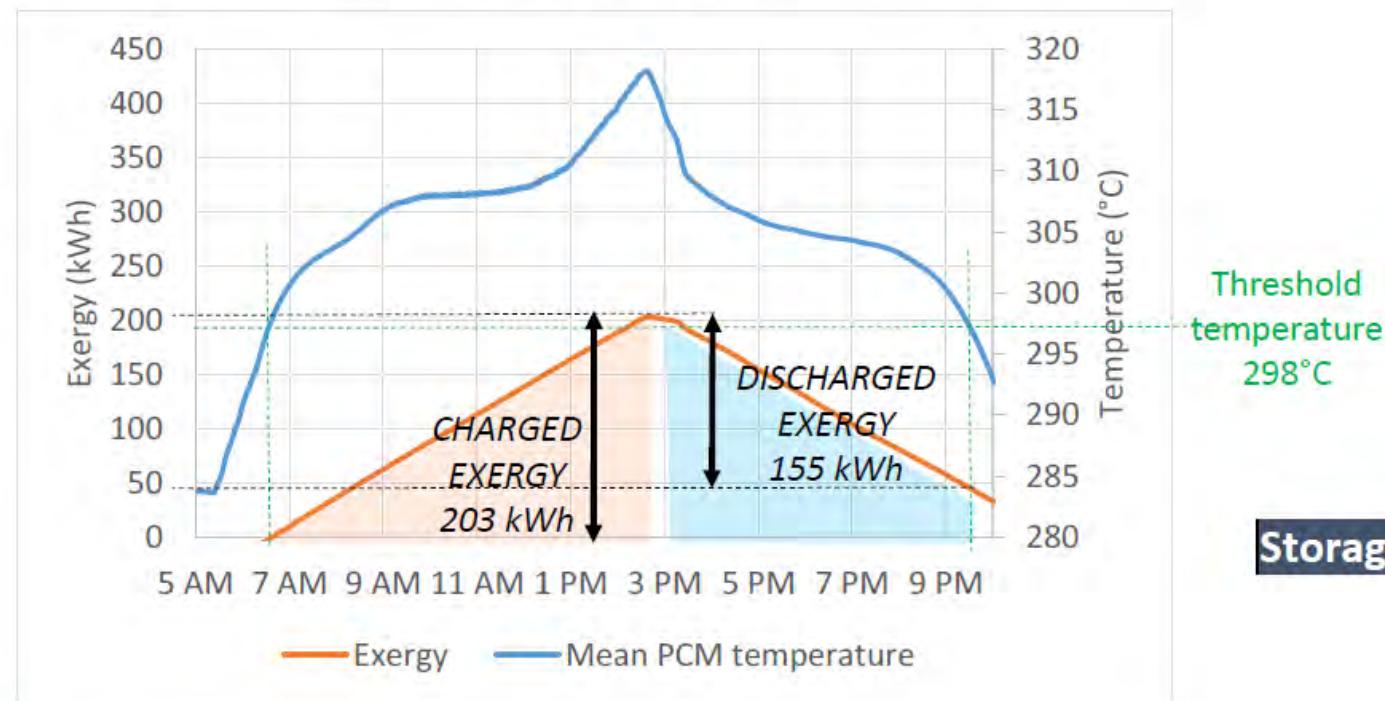
Ratio of energy gained by the HTF from the storage system during discharge to the energy delivered by the HTF during charge

- $\eta_{TES} = \frac{Q_{\text{discharge}}}{Q_{\text{charge}}} = \frac{Q_{\text{HTF\_out}}}{Q_{\text{HTF\_in}}}$  (In consecutive charge and discharge)
- $\eta_{TES}$  should be estimated in « cycling conditions »
  - With storage conditions at the end of discharge equal to those at the beginning of charge



Ratio of exergy gained by the HTF from the storage system during discharge to the energy delivered by the HTF during charge

- $\eta_{ex} = \frac{\epsilon_{discharge}}{\epsilon_{charge}} = \frac{\int_{discharge} \left(1 - \frac{T_0}{T_{discharge,out}}\right) dQ}{\int_{charge} \left(1 - \frac{T_0}{T_{charge,in}}\right) dQ}$  (In consecutive charge and discharge)
- $T_{charge,in}$  and  $T_{discharge,out}$  are usually measured by the same sensor

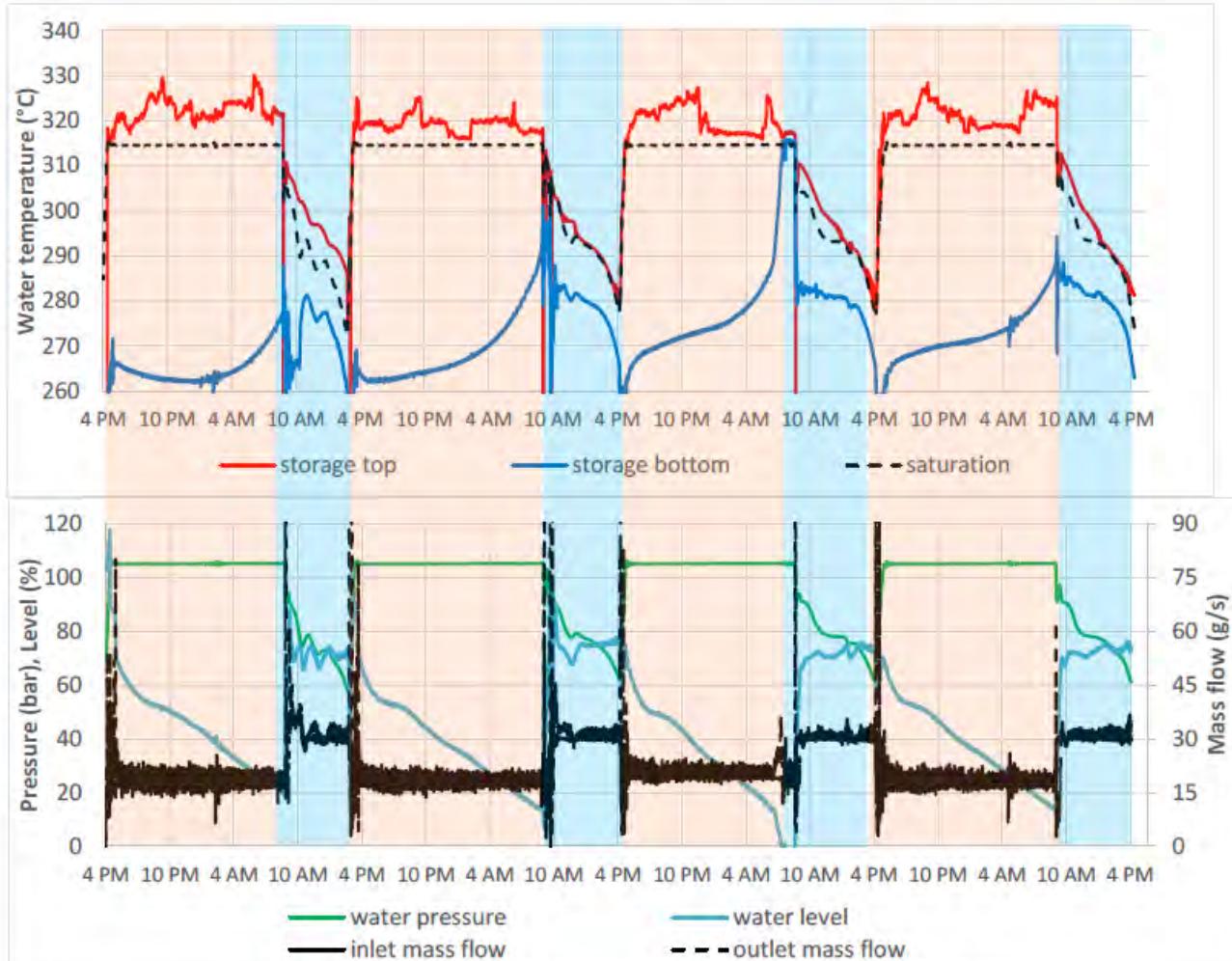
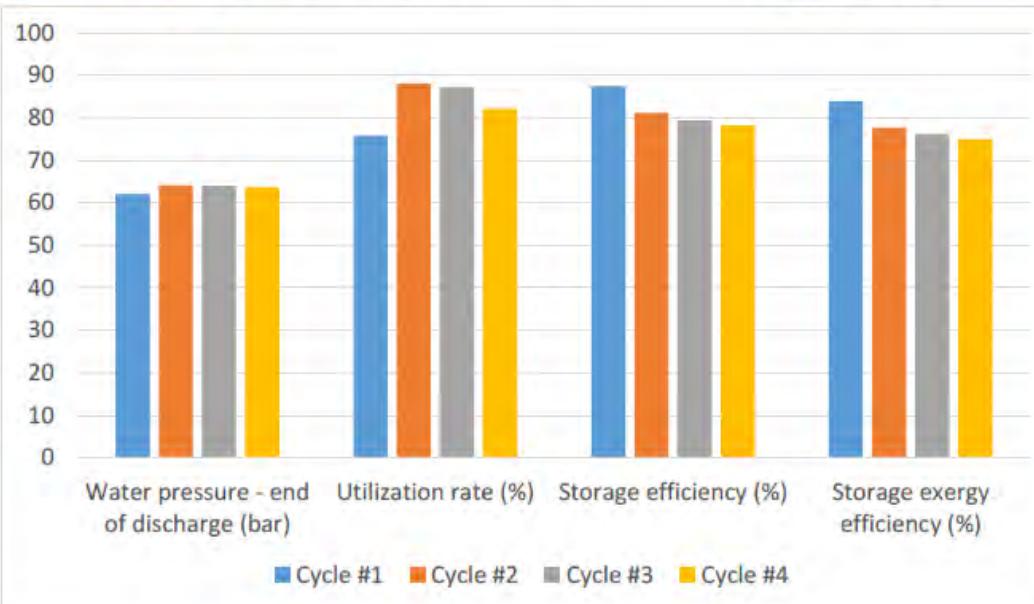


Storage exergy efficiency ( $\eta_{TES}$ ) | 76%

- **On the initial state**
  - Many KPIs vary depending on the initial state of the TES system
    - e.g. for thermocline TES, the initial state depends on previous charge-discharge cycles until stable initial conditions are reached
    - Less critical for LHTES (almost isothermal temperature at initial conditions)
  - To estimate storage efficiency in a fair way, “cycled initial conditions” are preferred
    - To have  $E_{start,charge} = E_{end,discharge}$  inside the tank
    - For latent heat storage , this criterion can be approached by looking at mean PCM temperature
- **On the start / end criteria**
  - KPI are evaluated on the HTF side, but you sometimes need information from inside the tanks...
    - Concept of storage level
  - For an operator in an industrial plant, end of charge/discharge criteria will be system-related
    - e.g. temperature threshold, pressure threshold, discharge duration,...
- **For one TES prototype, there is not a unique value for each KPI ( $\neq$  industrial standard)**
  - These guidelines mainly aims at pointing what should be clearly described for a fair and reproducible KPI evaluation

- Fixed pressure in charge, automated control during night
  - Thermal power: 25 kW<sub>th</sub> in charge, 50 kW<sub>th</sub> in discharge
  - 4 consecutive cycles

|                    | Criterion            | Threshold value                            |
|--------------------|----------------------|--|
| Start of charge    | PCM temperature      | $T_{mean} > 290 \text{ }^{\circ}\text{C}$  |
| End of charge      | Water level in tubes | $L_w < 17\%$                               |
| Start of discharge | Water flow direction | Valve positions in discharge configuration |
| End of discharge   | PCM temperature      | $T_{mean} < 290 \text{ }^{\circ}\text{C}$  |



THANK YOU FOR YOUR ATTENTION!  
ANY QUESTIONS?

